Engineering Evaluation of the
Human Research Facility
Refrigerated Centrifuge Prototype

Table of Contents

1.0	Acoustic Test	
1.1	Test Objective	
1.2	Test Procedure	3
1.3	Test Results	3
1.4	Conclusion	
2.0	Vibration Test	8
2.1	Test Objective	8
2.2	Test Procedure	
2	.1 Acceptance Random Vibration Test	9
2	.2 Qualification Acceptance Vibration Test	9
2.3	Test Results	9
2.4	Conclusion	9
3.0	Sinusoidal Resonance Survey	10
3.0	Sinusoidal Resonance Survey	10
3.1	Test Objective	10
3.2	Test Procedure	10
3.3	Test Results	
3.4	Conclusion	
4.1	Test Objective	
4.2	Test Procedure	
4.3	Test Results	
4.4	Conclusion	
5.0	Electromagnetic Interference Testing	
5.1	Test Objective	
5.2	Test Procedure	
5.3	Test Results	
-	.1 RE-02	
-	.2 CE-01	
-	.3 CE-03	
	.4 CE-07	
5.4		
	.1 RE-02	
_	.5 CE-01	
	.6 CE-03	
	.7 CE-07	
6.0	Duty Cycle Test	
6.1	Test Objective	
6.2	Test Procedure	
6.3	Test Results	
6.3	Conclusion	17

1.0 Acoustic Test

1.1 <u>Test Objective</u>

Test to verify if the test article can meet the space station requirement for acoustic emission. Test results can also help identify different noise sources for engineering evaluation.

1.2 <u>Test Procedure</u>

Acoustic Meter Data

Manufacture: CEL

Model Number: CEL-493; Calibration Number: M96511

Octave Filter Model Number: CEL-278; Calibration Number: M96511

Battery Check

A battery check should be performed prior to the test. Switch the meter from OFF to BAT and record the level below:

5.6 Volts.

Note: Batteries should be replaced if value is less than 3.4 volts.

A-Weighted Background Noise Check

Background Noise 33 dB(A)

Note: If the background noise exceeds 50 dB(A), then do not proceed with test until the noise level has been reduced to below that.

1.3 <u>Test Results</u>

Mode and Side Determination

Only front side will be monitored for this test. There are two different modes for testing:

Mode 1: Compressor On, Rotor at 2000 RPM

Mode 2: Compressor Off, Rotor at 2000 RPM

dB(A) Front: <u>63.5 dB(A)</u>, <u>Mode 1</u>

dB(A) when rotor at 14000 RPM: 81 dB(A)

Operator: Richard Yao Time: 5:00 am, Jan. 5, 2001

Table 1 shows the two feet measurement results for Mode 1 and Figure 1 shows the test result against the maximum allowed.

TABLE 1 TWO FEET MEASUREMENTS

COLUMN A CENTER FREQUENC Y (HZ)	COLUMN B BACKGROUND NOISE (dB LINEAR)	COLUMN C BACKGROUND NOISE + EXPERIMENT NOISE (dB LINEAR)	COLUMN D EXPERIMENT NOISE COLUMNS C - B (dB LINEAR)	COLUMN E FINAL CORRECTED EXPERIMENT NOISE (dB LINEAR)	COLUMN F MAXIMUM ALLOWED NOISE (dB LINEAR)
63	41.0	63.4	22.4	63.4	64
125	32.3	63.5	31.2	63.5	56
250	36.7	62.1	25.4	62.1	50
500	31.8	61.6	29.8	61.6	45
1000	31.3	56.1	24.8	56.1	41
2000	30.8	56.2	25.4	56.2	39
4000	32.2	52.4	20.2	52.4	38
8000	30.0	45.5	15.5	45.5	37

Mode: Mode 1

Front Side

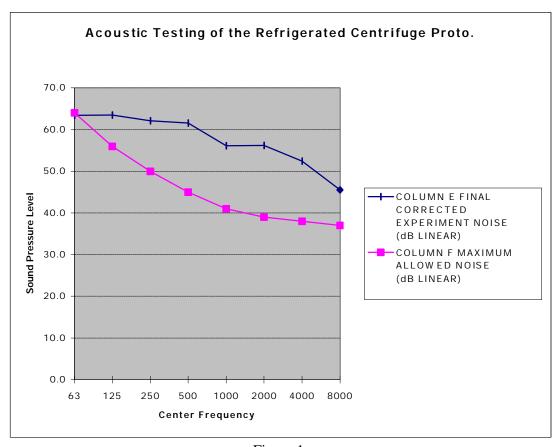


Figure 1

Table 2 shows the two feet measurement results for Mode 2 and Figure 2 shows the test result against the maximum allowed.

TABLE 2 TWO FEET MEASUREMENTS

COLUMN A CENTER FREQUENC Y (HZ)	COLUMN B BACKGROU ND NOISE (dB LINEAR)	COLUMN C BACKGROU ND NOISE + EXPERIMEN T NOISE (dB LINEAR)	COLUMN D EXPERIMENT NOISE COLUMNS C - B (dB LINEAR)	FINAL CORRECTE D EXPERIMEN T NOISE (dB LINEAR)	COLUMN F MAXIMUM ALLOWED NOISE (dB LINEAR)
63	41.0	63.4	22.4	63.4	64
125	32.3	63.5	31.2	63.5	56
250	36.7	62.1	25.4	62.1	50
500	31.8	61.6	29.8	61.6	45
1000	31.3	56.1	24.8	56.1	41
2000	30.8	56.2	25.4	56.2	39
4000	32.2	52.4	20.2	52.4	38
8000	30.0	45.5	15.5	45.5	37

Mode: Mode 2

Front Side

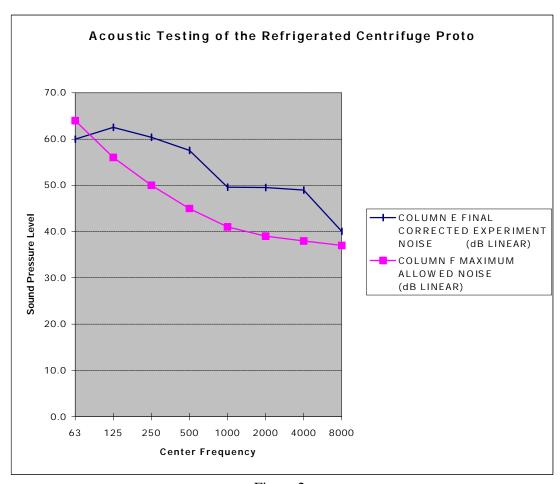


Figure 2

1.4 <u>Conclusion</u>

From the test results, it can be seen that although the overall noise level (63.5dBA) is lower than the maximum allowed for on ISS, for one hour operation (65dBA), the acoustic emission of the RC prototype exceeds the maximum allowed at every frequency range. It should also be noticed is that this test is done in an open environment rather than an enclosed rack, the noise from the common fans are overwhelming. Therefore, the test results cannot represent the rack mounted configuration.

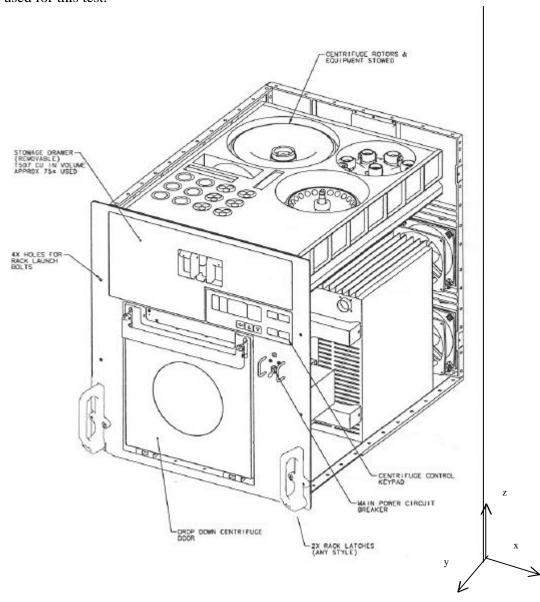
2.0 Vibration Test

2.1 <u>Test Objective</u>

The purpose of the vibration test is to test the structural integrity of the centrifuge design.

2.2 <u>Test Procedure</u>

The vibration test was performed at Marshall Space Flight Center in Huntsville Alabama per TPS 7E0020096, December 13th-14th, 2000. An Acceptance Vibration Test (AVT) and a Qualification Vibration Test (QAVT) were performed on the prototype unit. Diagram 2.2 illustrates the coordinate system used for this test.



2.2.1 Acceptance Random Vibration Test

The AVT test is done in all three axes for a duration of 60 seconds per axis. A full functional test was done before the start of the AVT, and at the conclusion of the AVT. Abbreviated functional test were performed in between each axis tested. Table 2.2.1 defines the test levels.

Table 2.2.1: AVT Test Levels

Frequency Range (Hz)	Minimum Power Spectral Density (g 2/Hz)
20	.010
20-80	+3.0
80-350	.04
350-2000	-3.0
2000	.007
Composite	6.1

2.2.2 Qualification Acceptance Vibration Test

The QAVT test is done in all three axes for a duration of 60 seconds per axis. A full functional test was done before the start of the AVT, and at the conclusion of the AVT. Abbreviated functional test were performed in between each axis tested. Table 2.2.2 defines the test levels.

Table 2.2.2: QAVT Test Levels

Frequency Range (Hz)	Minimum Power Spectral Density (g 2/Hz)
20	.017
20-80	+3.0
80-350	.087
350-2000	-3.0
2000	.012
Composite	7.9

2.3 Test Results

One anomaly was noticed after performing the z axis during the QAVT. The solenoid that is responsible for locking and unlocking the centrifuge door was stuck in the open position. This anomaly is due to a misalignment of the door and the lid locking mechanism. Other than this one anomaly, the prototype centrifuge successfully passed all other vibration testing.

2.4 Conclusion

The hardware performed exceptionally well during all vibration testing. The anomaly with the solenoid will be corrected by aligning the locking mechanism properly during assembly of the flight units.

3.0 Sinusoidal Resonance Survey

3.1 <u>Test Objective</u>

The purpose of the Sinusoidal Resonance Survey is to determine the fundamental resonance frequencies of the test article.

3.2 Test Procedure

The test was conducted in the x axis, at a sweep rate of one octave per minute from 5 to 200 Hz, one sweep up and down, with an input not to exceed 0.25 g zero to peak. An accelerometer was mounted the back left, bottom corner, at an accessible hard point on the centrifuge near the center of gravity (CG). The output of this response accelerometer was monitored so as not allow the hardware to experience more than 0.5 g peak. The input acceleration level shall be monitored by an accelerometer mounted as close as possible to the test fixture/hardware interface.

3.3 Test Results

The test shows that there is a resonance frequency at 7 Hz. The test had to be aborted at approximately 7 Hz due to a large spike in the accelerometer readout. The spike was a result of the internal components of the compressor resonating back and forth causing them to hit the internal wall of the compressor housing.

The input was decreased to 0.098 g, and the displacement was changed to 0.0767 inch and the test was restarted. Again, a loud banging was heard and the test was aborted. The test was restarted at the upper limit of 250 Hz, and run backwards, down the scale. This was done to determine the exact frequency at which the compressor was failing. It was determined to be 7 Hz. The data from this test is provided in an attachment labeled Appendix A.

3.4 Conclusion

The internal components of the compressor are mounted on springs. These springs are used to decrease the acoustic emission of the compressor. In an effort to correct the sinusoidal resonance frequency issues, a new design part will be added internal of the compressor housing incorporating springs to absorb the x and y energy. Figure 3-4 is a preliminary design that is being considered. In order to determine the best design solution, a sine sweep needs to be performed in the z axis.

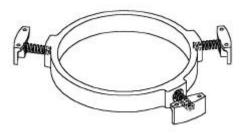


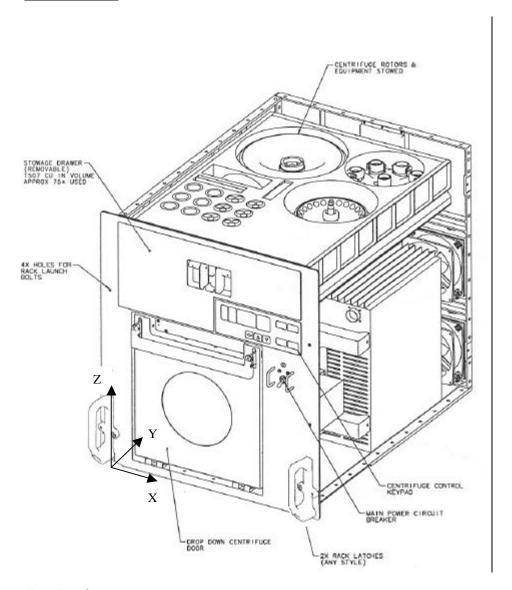
Figure 3.4: Spring Support Assembly

4.0 Weight and Center of Gravity

4.1 <u>Test Objective</u>

The purpose of the weight and cg test is to verify to verify that the weight and CG meet space station requirement. The results are also be used to verify the model used for the structural analysis.

4.2 <u>Test Procedure</u>



4.3 <u>Test Results</u>

The total weight of the prototype unit is 74.9 Kg (165.13 lbs). The maximum allowable weight for a 12 PU drawer is 87.09 kg (192 lbs).

The center of gravity is (20.49, 31.11, 22.19), in cm. The cg is within the allowable cg of a 12 PU drawer with 3 sets of slides.

4.4 <u>Conclusion</u>

The mass and cg of the unit are within the requirements as defined in the Program Requirements Document (LS71000).

5.0 Electromagnetic Interference Testing

5.1 <u>Test Objective</u>

The purpose of this test is to evaluate the levels of radiated and conducted emissions.

5.2 Test Procedure

The radiated emissions test, RE-02, and the conducted emissions tests, CE-01, CE-03, and CE-07 were performed in accordance with SSP30238 Rev D, per TPS 7E0020084. The results were compared to the limits of SSP 30237, Revision E. Documentation and complete testing charts are included in an attachment labeled Appendix B.

The chamber temperature was set to $-20 \deg C$ for continuous compressor operation, and the rotor speed was set to 6000 rpm. The test configuration is shown below in diagram 5.2.

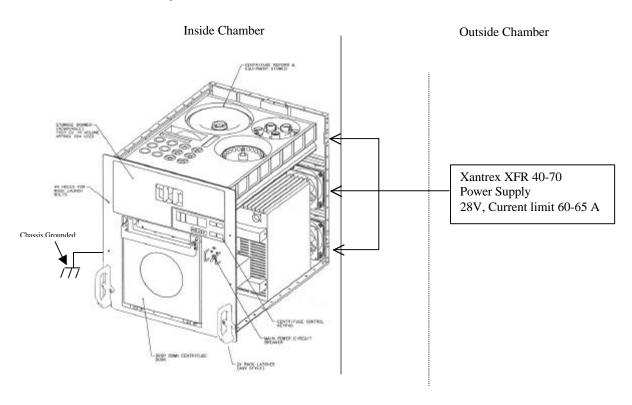


Figure 5.2: EMI Test Configuration

5.3 Test Results

5.3.1 RE-02

RE-02 measures the radiated emissions from a frequency range of 14 kHz to 15.5 GHz. EMI exceedances are documented as follows:

Frequency (MHz)	Amplitude (dBuv/m)	Exceedances ¹
0.01486	60.7	4.7
0.0152	62.4	6.4
0.01555	67.2	11.2
0.01614	66.3	10.3
0.0165	65.7	9.7

¹Exceedances are calculated from the amplitude versus the limits specified in SSP 30237, Revision E.

5.3.2 CE-01

CE-01 measures the conducted emissions on the hot and return leads of the HRF Centrifuge main power from a frequency range of 3 Hz to 15 kHz. No exceedances were observed from the test:

5.3.3 CE-03

CE-03 measures the conducted emissions on the hot and return leads of the HRF Centrifuge main power from a frequency range of 50 kHz to 50 MHz. The exceedances are documented as follows.

HOT LEAD					
Frequency (MHz)	Amplitude (dBuA)	Exceedances ¹			
0.07835	97.3	5.0			
0.1638	96.4	10.2			
RETURN LEAD					
Frequency (MHz)	Amplitude (dBuA)	Exceedances ¹			
0.07772	99.6	7.3			
0.1638	95.6	9.4			

¹Exceedances are calculated from the amplitude versus the limits specified in SSP 30237, Revision E.

5.3.4 CE-07

CE-07 measures the conducted emissions on start up transients of the HRF Centrifuge.

5.4 Conclusion

5.3.1 RE-02

An investigation of the EMI failure has been initiated and preliminary results indicate that the stowage drawer and centrifuge chamber drawer will need conductive coating and EMI gaskets to reduce radiated emissions of the HRF Centrifuge.

5.3.5 CE-01

Because the HRF Centrifuge did not demonstrate any failures for this test, no changes or modifications are required.

5.3.6 CE-03

Based upon the testing results, the HRF Centrifuge power filtering will need to be addressed. The most significant contribution to the CE-03 failure is during compressor operation that utilizes Pulse Width Modulation circuitry for inverter operation to operate the compressor. Proper filtering will be addressed and implemented into the flight design.

5.3.7 CE-07

Based upon the testing results, the HRF Centrifuge power filtering will need to be addressed. Current recommendation is to add appropriate LC circuits to smooth the startup transient.

6.0 Duty Cycle Test

6.1 <u>Test Objective</u>

The purpose of this test was to determine the on/off cycle of the compressor. This data is necessary for thermal and power analysis.

<u>6.2</u> <u>Test Procedure</u>

The rotor speed was set to 2000 RPM, and the chamber temperature was set to +4 °C. The test was performed for a duration of 30 minutes and the duration of each cycle was recorded. In addition to the cycle time, the compressor can temperatures and the internal door temperatures were recorded.

6.3 <u>Test Results</u>

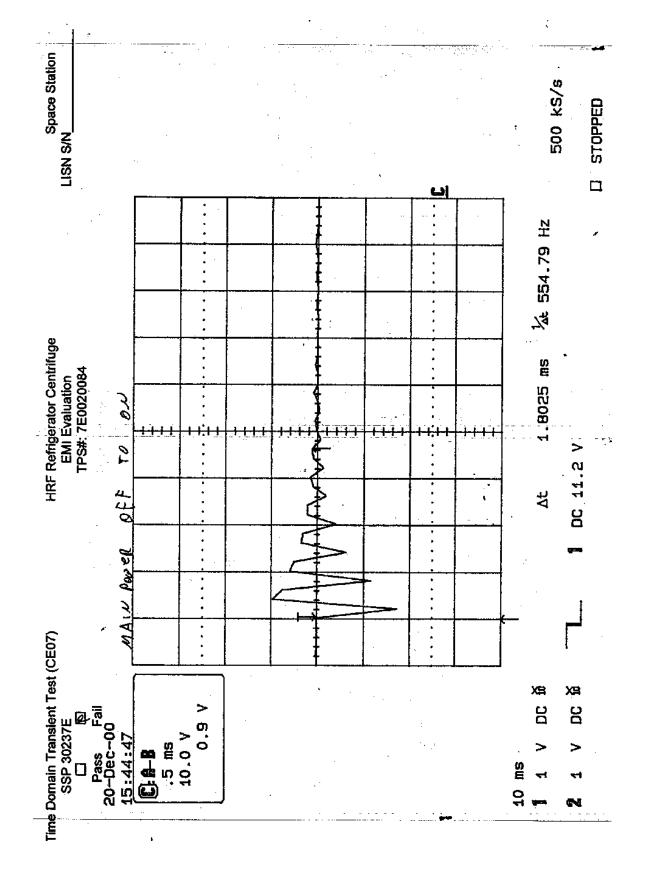
The test results are provided in Table 6.3.

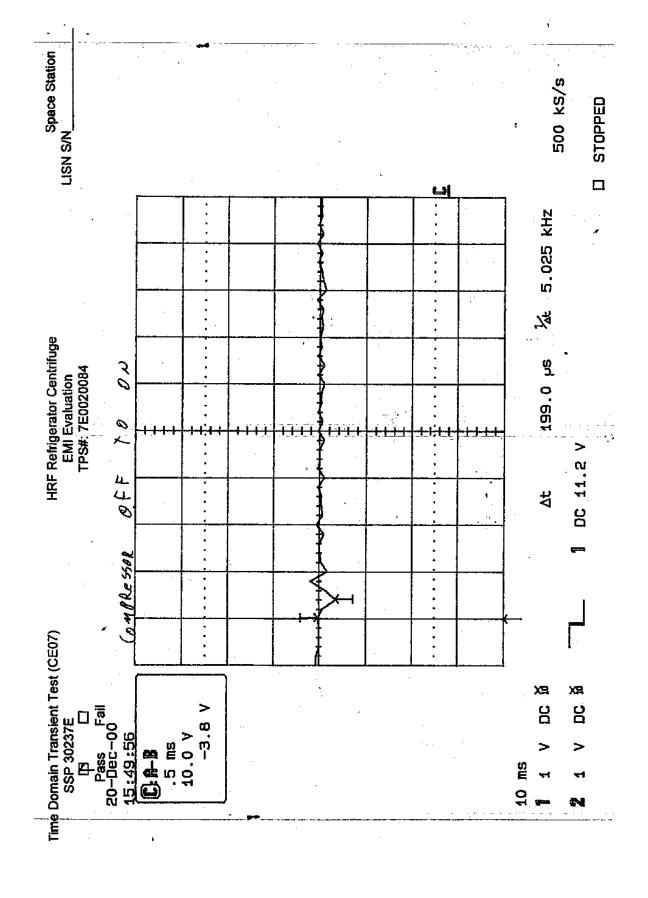
Table 6.3: Compressor Duty Cycle

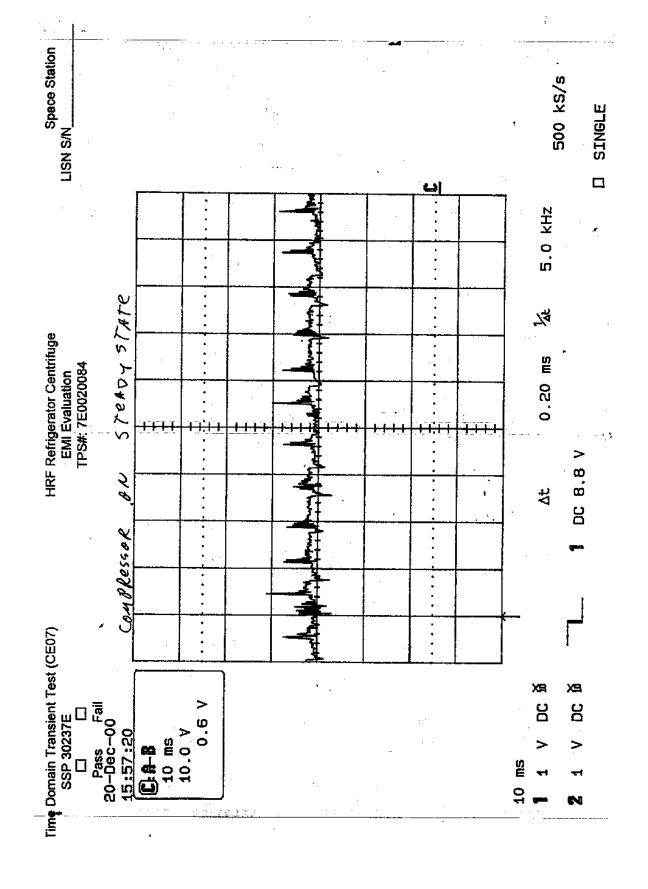
Duration (minutes)	Compressor On (minutes)	Compressor Off (minutes)	Outside door decal (C)	Outside Door Lexan (C)	Inside Door (C)	Compressor (C)
0:07:09	0:07:09		25.00	22.00	9.60	52.80
0:08:40		0:01:31				
0:11:05	0:02:25		25.00	22.00	8.70	54.30
0:12:03		0:00:58				
0:14:51	0:02:48		26.00	21.00	8.10	55.30
0:16:19		0:01:28				
0:18:36	0:02:17		25.00	21.00	7.70	55.60
0:20:06		0:01:30				
0:22:25	0:02:19		25.00	20.00	7.30	56.00
0:23:52		0:01:27				
0:26:15	0:02:23		25.00	20.00	7.10	57.70
0:27:43		0:01:28				
0:30:02	0:02:19		25.00	19.00	6.90	57.00

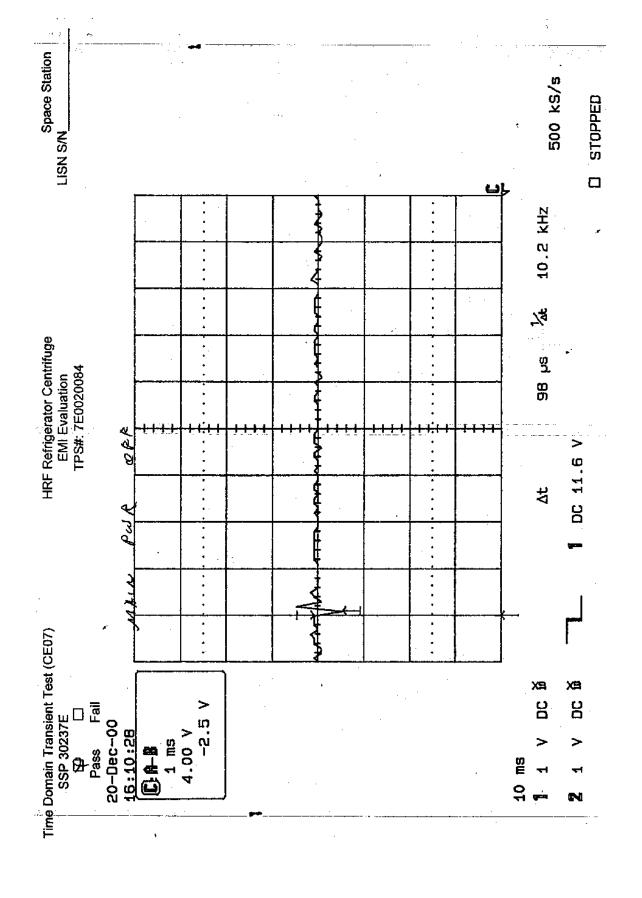
6.3 <u>Conclusion</u>

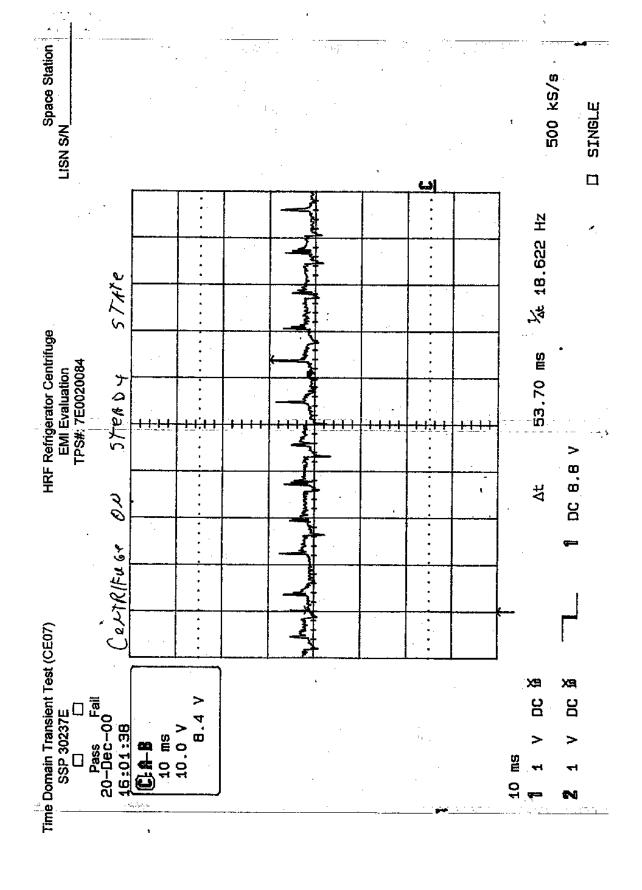
The compressor takes approximately seven minutes to cool the chamber to the desired temperature. The cool down rate is dependant on the rotor speed, and will cool down faster if the rotor is set to higher speeds. After the set temperature has been achieved, the compressor duty cycle is approximately 61%.

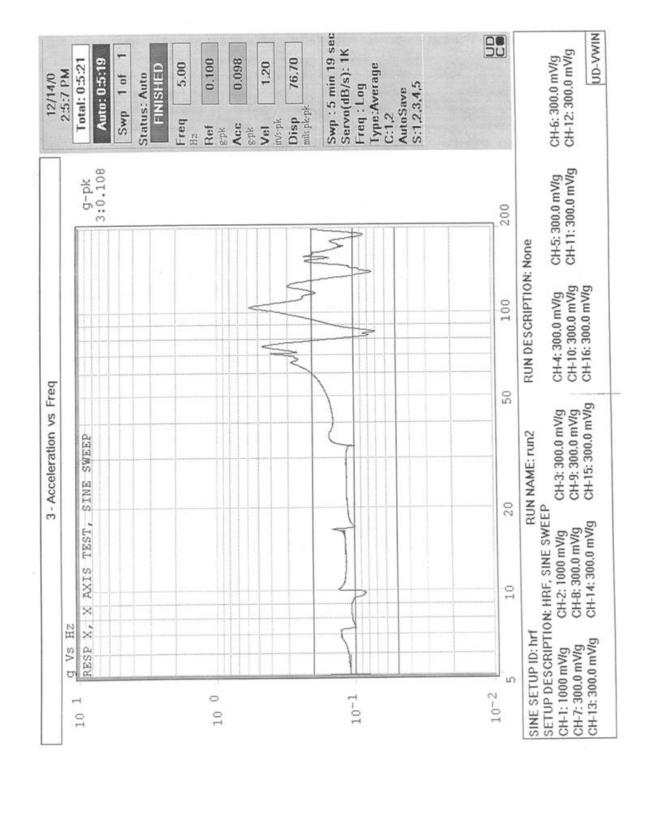


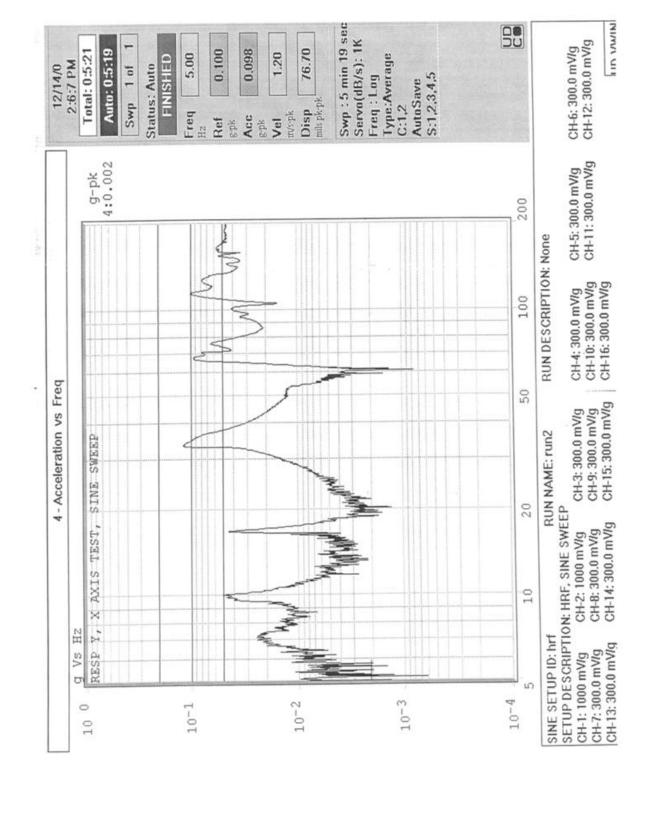


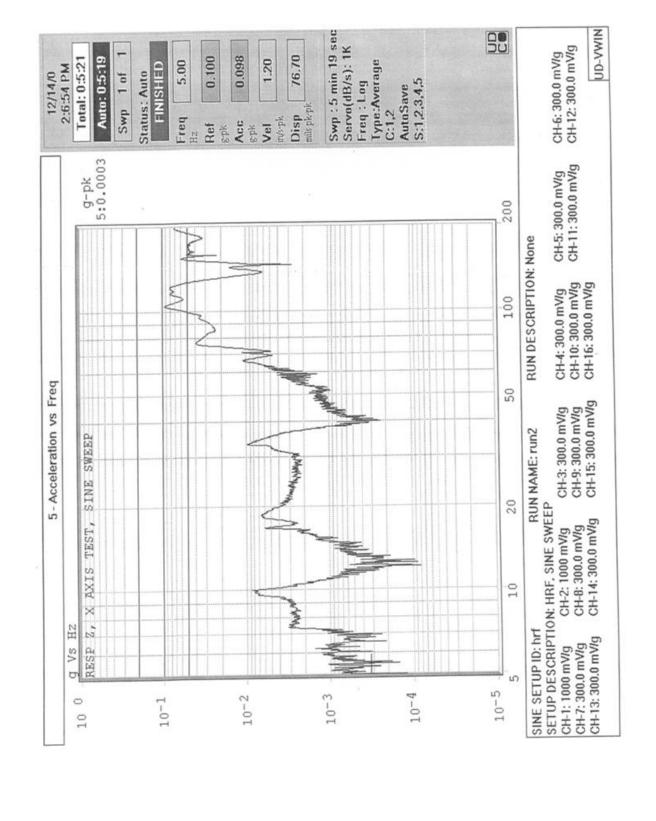


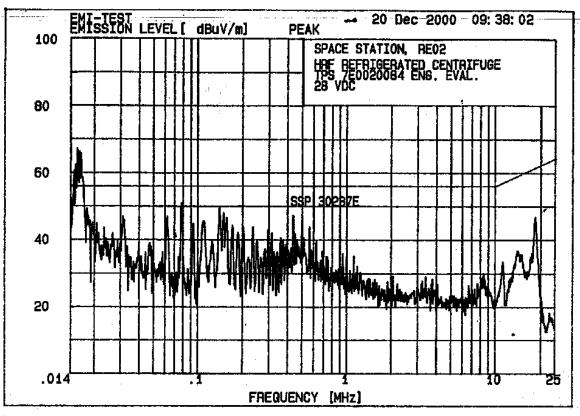


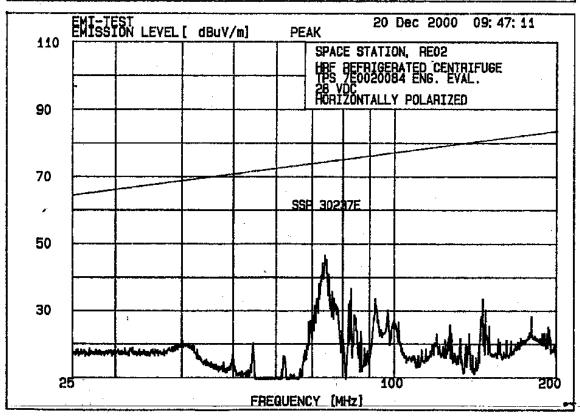


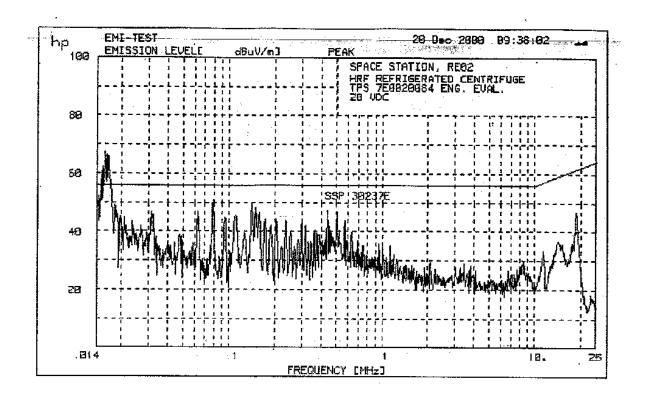












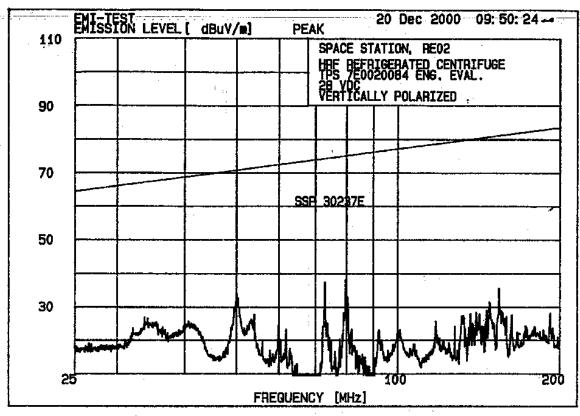
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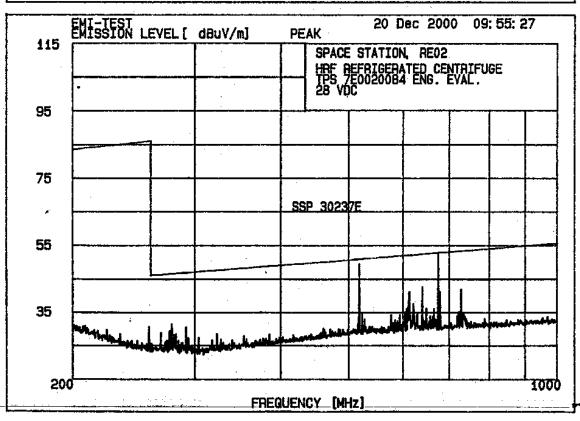
1. SPACE STATION EMISSIONS TESTS

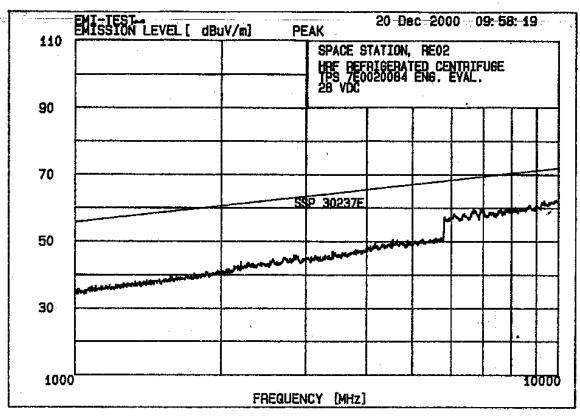
1.6 RE-02 -- 14KHZ TO 25MHZ

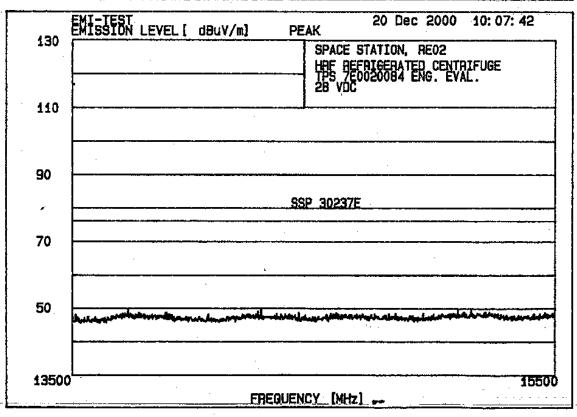
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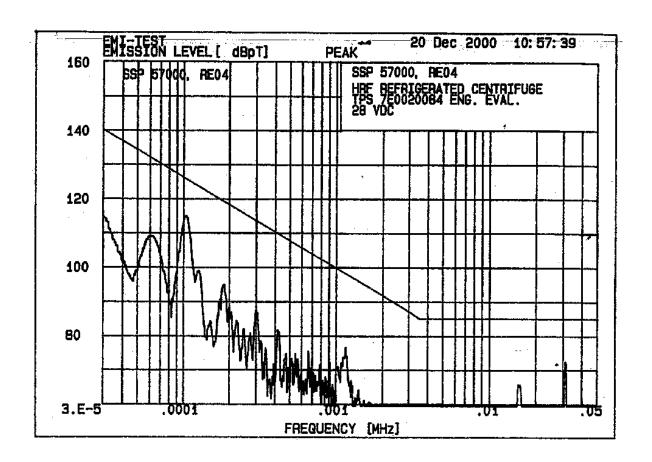
PEAK#	FREQ (MHz)	(dBuV/m)	DELTA
1	.01486	60.7	4.7
2	.0152	62.4	6.4
3	.01555	67.2	11.2
4	.01614	66.3	10.3
5	.0165	65.7	9.7



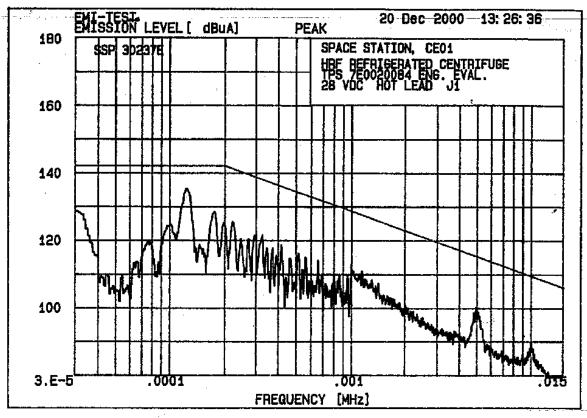


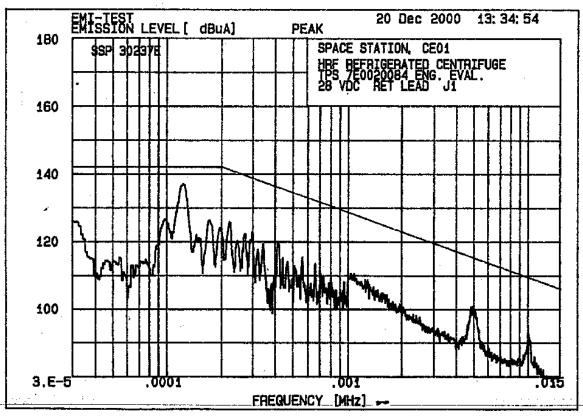


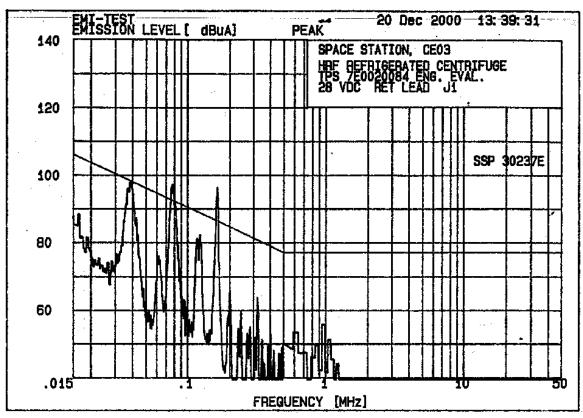


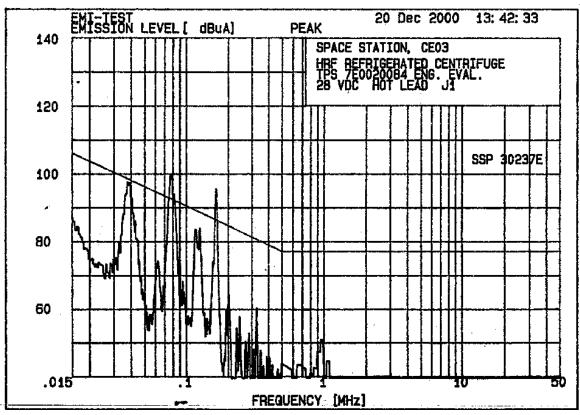


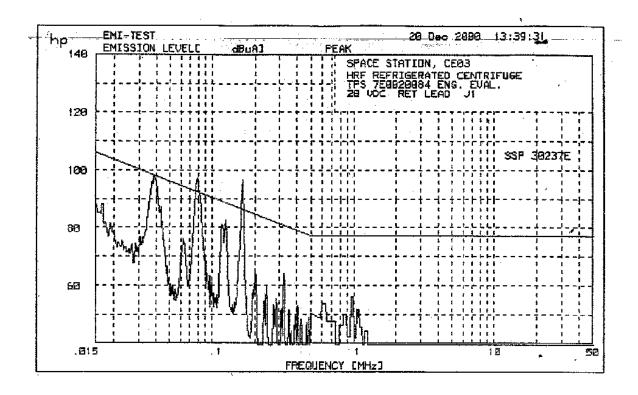
DC Magnetic Field Emission	uge Document No. 7E0020084 Tested By J.Wilkins Date Tested 12/20/00 Quality Status Evaluation		fer			Maximum Readings (dBpT)	146.02 dBpT (0.2 Gauss)
•	HRF Refrigerator Centrifuge SEE TPS SEE TPS N/A	DC Magnetic Field	F.W. Bell 9500 Gaussmete	7 cm		Maximun	146.02 d
	Component NASA Type No. NASA Serial No. Test Run Time	, '			Measurement Results		At lower right comer of centrifuge door











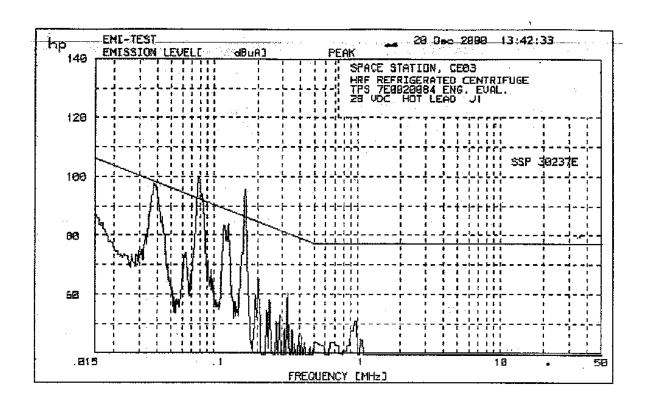
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1. SPACE STATION EMISSIONS TESTS

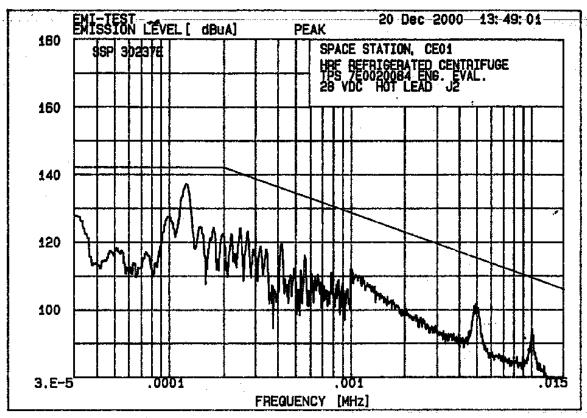
1.3 CE-03 -- 15KHZ TO 50MHZ

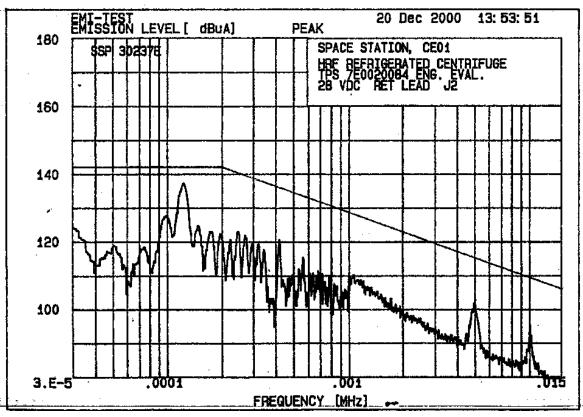
Peaks above 0 dB of Limit Line #1
peak criteria = 3 dB

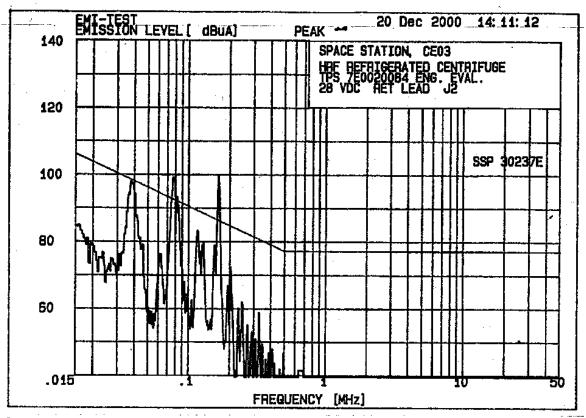
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2	.1638	96.4	10.2

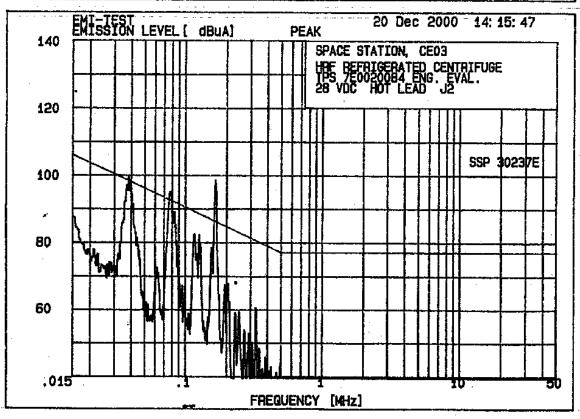


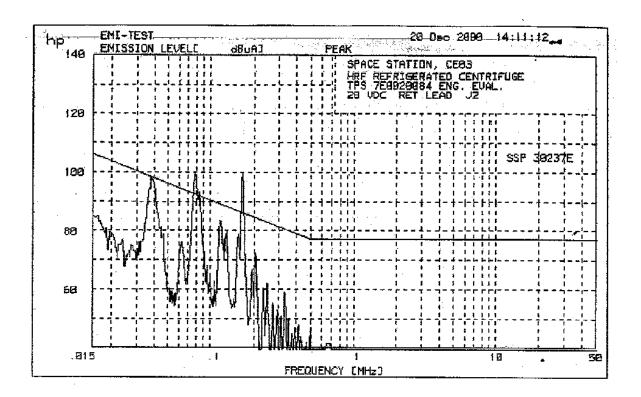
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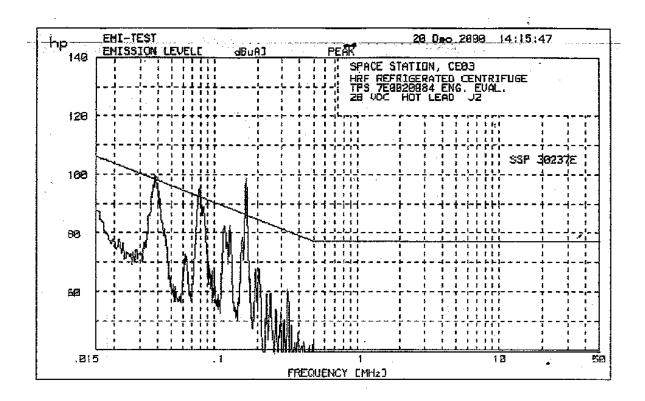




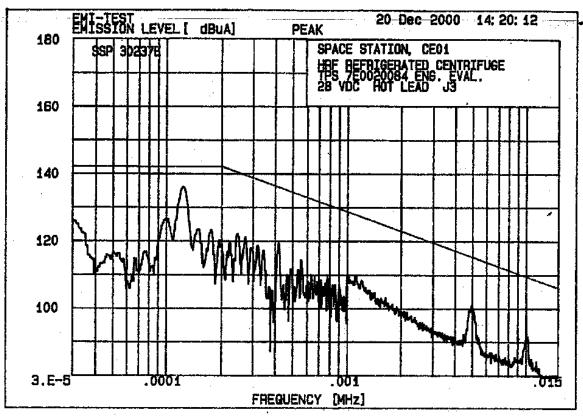


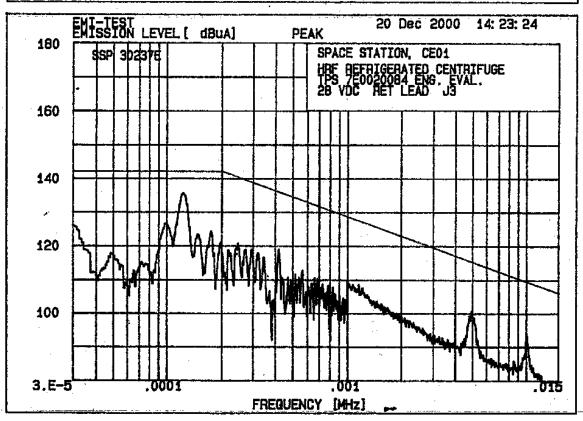


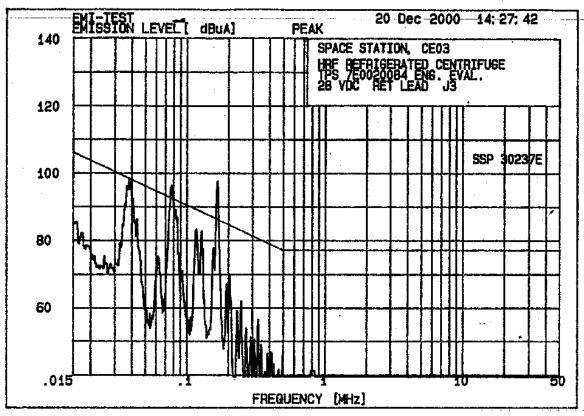
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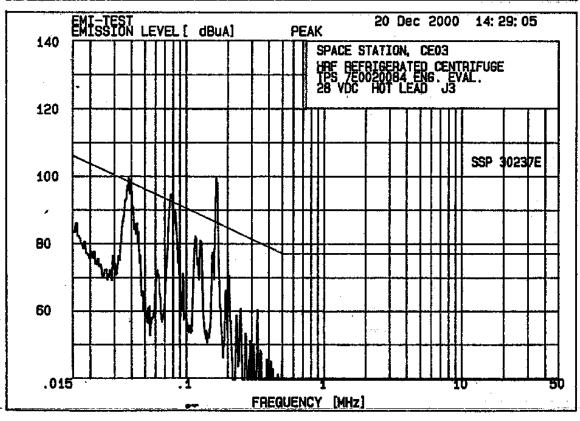


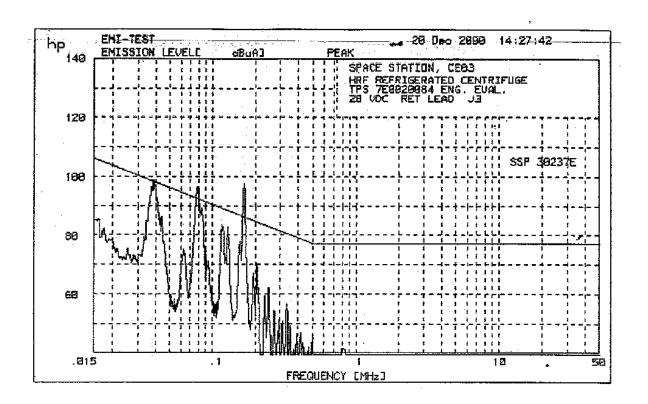
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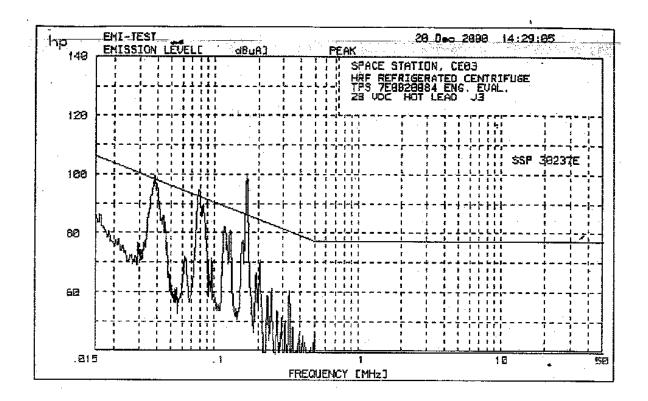








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PEAK# 1 2 3	FREQ (MHz) .0384 .07835 .1678	(dBuA) 98.6 96.3 97.6	DELTA .4 4.0 11.6	v. •



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1. SPA 1.9	CE STATION EMISS SPACE STATION			
======	:=====================================			
	bove 0 dB of Lin	mit Line #1		
	bove 0 dB of Lin criteria = 3 dB	mit Line #1		
peak		nit Line #1 (dBuA)	DELTA	
peak	criteria = 3 dB		DELTA 1.3	
	<pre>criteria = 3 dB FREQ (MHz)</pre>	(dBuA)		